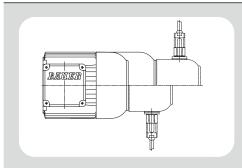
Energy Efficient Geared Motors AC Line Operated





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Functional description

The compression springs act on the anchor disc, which is free to move in the axial direction and presses the brake disc, which is keyed to the rotor shaft, against the friction plate or the motor bearing plate. This produces the braking torque.

When a DC voltage is applied to the coil in the electromagnet housing, it generates a magnetic force that opposes the spring force and causes the anchor disc to be pulled toward the electromagnet enclosure.

This releases the brake disc and disengages the brake.

Brakes are classified into two types according to how they are used: holding brakes and working brakes.

Holding brake ES.. / ZS..

brake that in normal operation does not convert kinetic energy into frictional energy but is only used to hold a mechanism in a particular position, but which can also be used for motion braking in an emergency.

Service brake ESX.. / ZSX..

A brake that converts kinetic energy into frictional energy in normal operation, which means that it brakes mechanical motion.

When a working brake is used as a holding brake, the braking torque tolerance of up to -30 % (in new condition) must be taken into account.

Product description of type ES(X) spring-actuated brakes

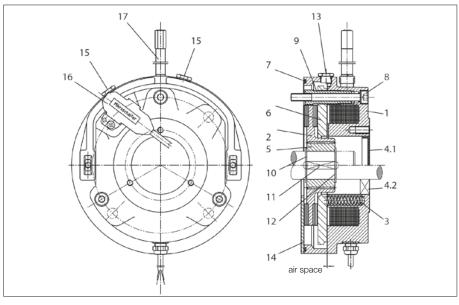


Figure 1: Construction of ES(X) brake

Construction of ES(X) brake

1 Electromagnet housing	9 Hollow screw	
2 Brake disc	10 Retaining ring	
3 Compression spring	11 Key	
4.1 Cover plate with closed brake	12 Retaining ring	
4.2 Shaft seal with through shaft	13 Screw plug for checking air gap	
5 Drive bush	14 Friction plate (only with motor size Dxx08 or Dxx09)	
6 Anchor disc	15 Screw plug for checking microswitch setting	
7 O-ring	16 Microswitch (optional)	
8 Fitting screw with copper washer	17 Manual release (optional)	7

Brake mounting

ES and ESX: Brake mounting is under the fan cover EH and EHX: Brake mounting is on the fan cover

Options

- Manual release, non-locking or locking
- Microswitch for monitoring operation or wear

Product description of type ZS(X) spring-actuated brakes

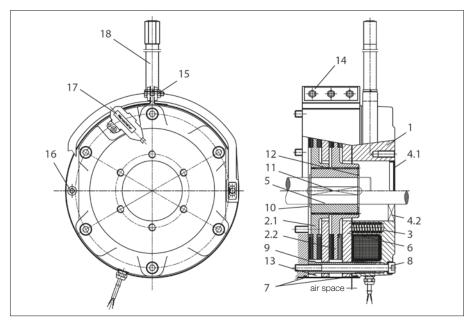


Figure 2: Construction of ZS(X) brake

Construction of ZS(X) brake

1 Electromagnet housing	9 Hollow screw
2.1 Brake disc	10 Retaining ring
2.2 Brake disc	11 Key
3 Compression spring	12 Retaining ring
4.1 Cover plate	13 Cover
4.2 Shaft seal with through shaft	14 Fitting screws
5 Drive bush	15 Bracket
6 Anchor disc	16 Assembly screw/assembly aid
7 O-ring	17 Microswitch (optional)
8 Fitting screw with copper washer	18 Manual release (optional)

Options

- Manual release, non-locking or locking
- Microswitch for monitoring operation or wear

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Brake selection and sizing

If the working brake is undersized, it will have increased wear and a shorter lifetime. If it is oversized, the resulting mechanical forces may overload the drive.

If specific application data is not available, in the case of horizontally driven equipment we recommend selecting a braking torque with a safety factor (K) of 1 to 1.5 times the rated torque of the motor.

For braking to standstill, the selected braking torque should be at least 80 % of the rated torque of the drive.

Rated torque:

$$M_{Berf} = \frac{P \times 9550}{n_2} \times K$$

MBerf	Braking torque	[Nm]
Ρ	Motor power	[kW]
n	Rated speed at rotor shaft	[rpm]

For lifting operation, a braking torque equal to twice the rated motor torque should always be chosen for safety reasons.

If the moment of inertia, speed and allowable deceleration time of the machine are known, the braking torque can be calculated as described below.

External moments of inertia

If the masses to be decelerated by the brake do not run at the same speed as the rotor shaft, the moment of inertia (J_{ext}) must be reduced to the value at the rotor shaft

$$J_{\text{ext}} = \frac{J_{\text{ext}1} \times n_1^2 + J_{\text{ext}2} \times n_2^2 + \dots + J_{\text{ext}n} \times n_n^2}{2}$$

or the external moment of inertia reduced by the gear ratio of the gear unit to the value at the rotor shaft.

$$J_{ext'} = \frac{J_{ext}}{i^2}$$

J_{ext} Total external moment of inertia [kgm²]

- J_{ext}' Total external moment of inertia referenced to the rotor shaft [kgm²]
- J_{ext1,2,...} Individual external moments of inertia [kgm²]
- i Gear reduction ratio
- n Rotor shaft speed
- n_{1,2}... Speeds of the individual moments of inertia [rpm]

Load torque under static load

$M_{L} = F x r$

M∟ Load torque [Nm]

- F Force [N]
- r radius [m]

Braking torque with dynamic load

A purely dynamic load is present when flywheels, rolls, etc. must be decelerated and the static load torque is negligible.

$$M_{a} = \frac{J_{ges} \times n_{a}}{9,55 \times (t_{a} - t_{A})} = \frac{(J_{ext'} + J_{rot} + J_{Br}) \times n_{a}}{9,55 \times (t_{a} - t_{A})}$$

Moment of inertia of the brake [kgm²] Jbr

- Moment of inertia of the rotor shaft and rotor [kgm²] J_{rot}
- Ma Deceleration torque [Nm]
- Initial speed at start of deceleration [rpm] na
- Total deceleration time (from switch-off until drive is stationary) [s] ta
- The response time of the brake for braking corresponds to t_{AC} or t_{DC} tΑ in the specification tables [s]

Dynamic and static loads

In most application situations, both static and dynamic loads are present.

 $M_{Berf} \leq M_{Br}$ $M_{Berf} = (M_a \pm M_I) \times K$ where must hold true.

braking (positive) or driving (negative) load torque [Nm] M∟

Heat generated by each brake cycle

Friction converts the kinetic energy of the moving masses into heat.

This amounts to

W =	$\frac{J_{ges} \times n^2}{182,5} =$	$\frac{(J_{ext'} + J_{rot} + J_{Br}) \times n_a^2}{182,5}$	where	$W \leq W_{max}$	must hold true.
W Mmax		Braking energy for eac Maximum permissible f (see brake tables)			e cycle

Thermally allowable braking energy of working brakes

With a uniform sequence of brake cycles, which means a certain average number of brake cycles per hour, the temperature rises until an equilibrium between heat input and heat dissipation is reached. The temperature rise must be sized to avoid overheating the coil and the friction layer, taking the ambient temperature into account.

Braking to standstill:

 $W_{z} = W \times Z \leq W_{th}$

- Wth Maximum allowable braking energy per hour
- Wz Braking energy with Z brake cycles
- Z Number of brake cycles per hour

Lifting operation

In lowering operation, the drive motor acts as a generator and its braking effect results in a steady downward motion (constant speed). If we ignore transmission losses, under full load the drive must brake the load with the rated motor torque. If a mechanical brake with a braking torque equal to the braking torque of the motor is applied after the drive is switched off, the downward motion will continue at the same speed. This means that additional braking torque is necessary to stop the motion of the load. For example, if the brake is dimensioned for 200 % braking torque, approximately 100 % is used for "static" deceleration and the rest is used for "dynamic" deceleration.

If part of the braking torque is required for braking the load during lowering (downward motion), the brake engagement time is greater, and the thermal load is therefore greater.

In this case

$$W_{_{H}} = \frac{M_{_{Br}}}{M_{_{Br}} - M_{_{L}}} \times W_{_{Z}}$$

 W_H Friction energy per hour in lifting operation M_{Br} Braking torque of the brake

Brake lifetime

The energy absorbed during braking causes the brake disc to wear, which increases the air gap. If the air gap increases beyond a certain maximum gap size, the magnetic field is so weak that the pulling force of the electromagnet is no longer sufficient to release the brake. A proper air gap must be restored by adjusting the air gap or by replacing the brake disc, depending on the type of brake construction.

The maximum number of brake cycles until service is necessary can be calculated as follows:

$$Z_L = \frac{W_L}{W}$$

ZL Number of brake cycles until the air gap limit is reached

WL Maximum allowable braking energy until maintenance; i.e. replacing the brake disc or adjusting the air gap. Adjustment of the air gap is possible only with type ZXSxx brakes.

Deceleration time

The pure braking time from the start of mechanical braking to standstill depends on the braking deceleration.

Especially with lifting operation, but also in other types of operation, it is necessary to check whether the load torque reinforces the braking effect or counters the braking effect.

The deceleration time is therefore calculated as follows:

$$t_{a} = \frac{J_{ges} \times n_{a}}{9,55 \times (M_{er} \pm M_{I})}$$

Electrical connection

General

There are two basic options for providing the supply voltage for the DC electromagnet:

- 1. Externally from an existing DC control voltage mains or a rectifier in the cabinet.
- 2. From a rectifier built into the motor or brake terminal box. In this case, the rectifier can be powered either directly from the motor terminal board or from the mains.

Note that in the following cases the rectifier is not allowed to be connected to the terminal board of the motor:

- Pole-changing motors and motors with wide operating voltage range
- Operation from a frequency converter
- Other configurations in which the motor voltage is not constant, such as operation with soft-start devices, start-up transformers, etc.

Release

When the rated voltage is applied to the electromagnet coil, the current through the coils increases exponentially and with it the generated magnetic field. The current must rise to a certain value (Irelease) before it overcomes the spring force and starts to release the brake.

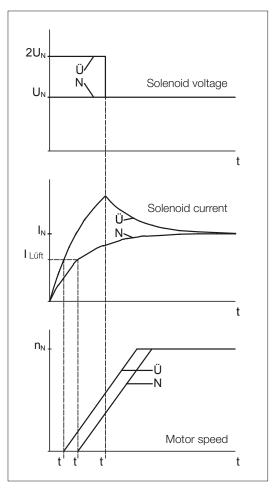


Figure 3: Idealised curves of coil voltage, coil current and motor speed with normal excitation (N) and overexcitation (Ü). tu: overexcitation time; tan, tau: Response time with normal excitation and overexcitation. Two different situations can arise during the response time tA, assuming that the voltage is applied to the motor and the brake simultaneously:

- The motor is locked if M_A < M_L + M_{Br} The motor draws its locked-rotor current, which increases the thermal load on the motor. This situation is illustrated in Figure 3.
- The brake slips if $M_A > M_I + M_{Br}$
- In this case, the brake is also thermally stressed during start-up and wears faster.

MA: locked rotor torque of the motor; ML: load torque; MBr: braking torque

As can be seen, there is an additional load on the motor and brake in both cases. The effect of the response time increases with increasing brake size. Consequently, it is advisable to reduce the response time, especially with medium-sized and large brakes and with a high cycle rate. This can be achieved relatively easily by means of electrical overexcitation. With this approach, the coil is briefly operated at twice its rated voltage after switch-on.

This causes the current to rise faster than with normal excitation, and it reduces the response time by approximately 50 %. This overexcitation function is built into the type MSG special rectifier.

The release current increases with increasing air gap, and with it the response time. When the release current exceeds the rated coil current, the brake will not be released with normal excitation and the brake has reached its wear limit.

Braking

The brake does not start generating braking torque immediately after the coil voltage is switched off. First the magnetic energy must decline to the point that the spring force can overcome the magnetic force. This occurs at the holding current I_{hold} , which is lower than the release current.

The response time depends on how the voltage is switched off.

Switching off the AC supply voltage to a type SG standard rectifier

- a) Rectifier powered from the motor terminal board (Figure 4, curve 1) Response time t_{A1}: very long
- Cause: Due to the residual magnetism of the motor, after the motor voltage is switched off a slowly decaying voltage is induced, and it continues to supply power to the rectifier and thereby to the brake. In addition, the magnetic energy of the brake coil is dissipated relatively slowly in the freewheel circuit of the rectifier.
- b) Rectifier powered separately (Figure 4, curve 2) Response time t_{A2} : long
- Cause: After the rectifier voltage is switched off, the magnetic energy of the brake coil is dissipated relatively slowly in the freewheel circuit of the rectifier.

If the supply voltage is interrupted on the AC side, no significant switch-off voltage occurs on the electromagnet coil.

Interrupting the DC circuit of the electromagnet coil (Figure 4, curve 3)

- a) By a mechanical switch
- with separate power supply from a DC control voltage mains or
- at the DC switch contacts (A2 and A3) of the type SG standard rectifier Response time t_{A3}: very short
- Cause: The magnetic energy of the brake coil is dissipated very quickly by arcing across the switch contacts.

b) Electronic

Using a type ESG or MSG special rectifier

Response time ta3: short

Cause: The magnetic energy of the brake coil is dissipated quickly by a varistor integrated in the rectifier.

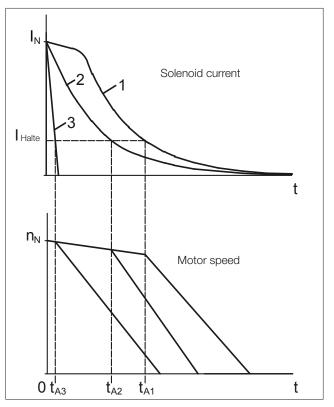


Figure 4: Idealised coil current and motor speed curves after switching off power on the AC side (1 and 2) or DC side (3)

If the circuit is interrupted on the DC side, a high voltage u_q is induce by the electromagnet coil. The magnitude of this voltage depends on the inductance L of the coil and the switch-off speed di/dt according to the formula

 $u_q = L \cdot \frac{di}{dt}$

Due to the winding design, the inductance L increases with increasing rated coil voltage. Consequently, the voltage spikes induced at switch-off can reach hazardous levels with relatively high coil voltages. For this reason, a varistor is included in the circuit for all brakes with voltages greater than 24 V.

This varistor is solely intended to protect the electromagnet coil; it is not intended to protect adjacent electronic components or devices against electromagnetic interference. On request, brakes with rated voltages of 24 V or less can also be fitted with a varistor.

If the circuit is interrupted on the DC side by a mechanical switch, the resulting arcing over the switch contacts causes strong erosion of the contacts. For this reason, only special DC contactors or adapted AC contactors with contacts rated for use class AC3 as specified in EN 60947-4-1 may be used.

Specifications of holding brakes with emergency stop capability

The maximum allowable friction energy values stated here do not apply to brake motors for use in areas with potentially explosive atmospheres.

Refer to separate data in appropriate documents for explosion-proof drives.

Туре	M_{Br}	W _{max}	W _{th}	W_{L}	tA	t _{AC}	t _{DC}	Pel	J
	[Nm]	[10 ³ J]	[10 ³ J]	[10 ⁶ J]	[ms]	[ms]	[ms]	[W]	[10 ⁻³ kgm ²]
E003B9	3	1.5	-	-	35	150	15		
E003B7	2.2	1.8	-	-	28	210	20	20	0.01
E003B4	1.5	2.1	-	-	21	275	30		0.01
E004B9	5	2.5	-	-	37	125	15		
E004B8	4	3	-	-	30	160	18	-	
E004B6	2.8	3.6	-	-	23	230	26	30	0.017
E004B4	2	4.1	-	-	18	290	37		
E004B2	1.4	4.8	-	-	15	340	47	-	
ES/EH010AX	15*	3	-	-	110	-	30		
ES/EH010A9	10	3	-	-	60	100	15	-	
ES/EH010A8	8	3	-	-	55	150	20	05	0.045
ES/EH010A5	5	3	-	-	45	220	20	35	0.045
ES/EH010A4	4	3	-	-	30	250	20	1	
ES/EH010A2	2.5	3	-	-	25	350	25	1	
ES027AX	32*	2.5	-	-	80	-	30		
ES/EH027A9	27	2.5	-	-	120	100	15		0.470
ES/EH027A7	20	2.5	-	-	100	130	20	50	0.172
ES/EH027A6	16	2.5	-	-	80	170	25	-	
ES/EH040A9	40	3.5	-	-	100	100	20		
ES/EH040A8	34	3.5	-	-	80	200	25	65	0.45
ES/EH040A7	27	3.5	-	-	70	250	30		
ES/EH070AX	90*	3.5	-	-	120	-	40		0.86
ES/EH070A9	70	3.5	-	-	120	150	18		
ES/EH070A8	63	3.5	-	-	120	200	20	85	
ES/EH070A7	50	3.5	-	-	90	220	25		
ES/EH125A9	125	4.5	-	-	170	220	25		
ES/EH125A8	105	4.5	-	-	150	320	28		
ES/EH125A7	85	4.5	-	-	135	350	30	105	1.00
ES/EH125A6	70	4.5	-	-	120	440	35	105	1.22
ES125A5	57	4.5	-	-	100	600	40		
ES125A3	42	4.5	-	-	90	700	45	1	
ES/EH200A9**	200	8	-	-	400	150	22		
ES/EH200A8**	150	8	-	-	280	250	35	105	2.85
ES/EH200A7**	140	8	-	-	200	320	35	1	
ES250A9**	250	9	-	-	300	500	45		
ES250A8**	200	9	-	-	200	960	60	1	
ES250A6**	150	9	-	-	160	1100	60	135	6.65
ES250A5**	125	9	-	-	150	1500	90]	
ES250A4**	105	9	-	-	130	1800	110		
ZS300A9**	300	8	-	-	280	220	35	75	5.7
ZS300A8**	250	8	-	-	210	380	45	10	0.7
EH400A9**	400	10	-	-	300	600	60		
EH400A7**	300	10	-	-	200	850	75	180	19.5
EH400A5**	200	10	-	-	150	1400	85	1	
ZS500A9**	500	9	-	-	320	320	50	100	10.0
ZS500A8**	400	9	-	-	260	600	60	100	13.3

** Cannot be combined with PMSM motors of the S series

Braking torque tolerance: -10 / +30 %

 W_{th} and WL are not specified because little or no braking energy is dissipated by holding brakes when they are used as intended.

For versions with braking torque marked with *, which may only be used with an MSG rectifier, the values of t_{A} and t_{DC} apply to operation with an MSG rectifier; i.e. t_{A} for overexcitation or t_{DC} for electronic circuit interruption on the DC side.

Due to the effects of operating temperature and manufacturing tolerances, actual response times may differ from the guideline values listed here.

Specifications of working brakes

The maximum braking energy values stated here do not apply to brake motors for use in areas with potentially explosive atmospheres.

Refer to separate data in appropriate documents for explosion-proof drives.

Туре	M_{Br}	W _{max}	W _{th}	W W	L	t _A	t _{AC}	t _{DC}	P _{el}	J
	[Nm]	[10 ³ J]	[10 ³ J]	[106	J]	[ms]	[ms]	[ms]	[W]	[10 ⁻³
				without HL***	with HL***	L -1		L - J		kgm ²]
003B9	3	1.5	36	55	55	35	150	15		
003B7	2.2	1.8	36	90	90	28	210	20	20	0.01
003B4	1.5	2.1	36	140	140	21	275	30		0.01
004B9	5	2.5	60	50	50	37	125	15		
004B8	4	3	60	100	100	30	160	18	-	
004B6	2.8	3.6	60	180	180	23	230	26	30	0.017
004B4	2	4.1	60	235	235	18	290	37		0.017
004B2	1.4	4.8	60	310	310	15	340	47		
SX/EHX010AX	15*	3	250	120	120	110	-	30		
SX/EHX010A9	10	3	250	120	120	60	100	15	1	
SX/EHX010A8	8	3	250	150	150	55	150	20	1	
SX/EHX010A5	5	3	250	240	240	45	220	20	35	0.045
SX/EHX010A4	4	3	250	300	240	30	250	20		
SX/EHX010A2	2.5	3	250	390	240	25	350	25	1	
SX027AX	27*	10	350	150	150	80	-	30		
SX/EHX027A9	22	10	350	150	150	120	100	15		0.470
SX/EHX027A7	16	10	350	300	300	100	130	20	- 50	0.172
SX/EHX027A6	13	10	350	350	350	80	170	25		
SX/EHX040A9	32	20	450	420	420	100	100	20		
SX/EHX040A8	27	20	450	560	490	80	200	25	65	0.45
SX/EHX040A7	22	20	450	700	490	70	250	30		
SX/EHX070AX	72*	28	550	700	700	120	-	40		
SX/EHX070A9	58	28	550	500	500	120	150	18	1 05	
SX/EHX070A8	50	28	550	800	700	120	200	20	85	0.86
SX/EHX070A7	40	28	550	1200	700	90	220	25	1	
SX/EHX125AX	100*	40	700	1900	1900	100	-	70		
SX/EHX125A9	85	40	700	1700	1700	150	320	28	1	
SX/EHX125A8	70	40	700	1900	1700	135	350	30	105	1 00
SX/EHX125A7	58	40	700	2700	1700	120	440	35	105	1.22
SX125A5	45	40	700	3300	1700	100	600	40]	
SX125A3	34	40	700	3300	1700	90	700	45]	
SX/EHX200AX**	160*	60	850	2000	2000	105	-	70		
SX/EHX200A9**	120	60	850	1700	1700	280	250	35	105	2.85
SX/EHX200A8**	110	60	850	2600	2600	200	320	35]	
SX250A9**	200	84	1000	2800	2800	300	500	45		
SX250A8**	160	84	1000	6800	5700	200	960	60]	
SX250A6**	120	84	1000	8500	5700	160	1100	60	135	6.65
SX250A5**	100	84	1000	11000	5700	150	1500	90		
SX250A4**	85	84	1000	11000	5700	130	1800	110		
SX300A9**	250	60	850	1300	1300	280	220	35	75	5.7
SX300A8**	200	60	850	2000	2000	210	380	45	10	0.7
HX400A9**	320	120	1100	3000	3000	300	600	60		
HX400A7**	240	120	1100	4800	4800	200	850	75	180	19.5
HX400A5**	160	120	1100	6000	4800	150	1400	85		
SX500A9**	400	84	1000	2800	2800	320	320	50	100	13.3
SX500A8**	320	84	1000	4000	4000	260	600	60	100	10.0

*** HL = manual release

Braking torque tolerance:

E003 / E004: -10 / +30 %

ESXxx / ZSXxx: -20 / +30 % after run-in; up to -30 % in new condition.

For versions with braking torque marked with *, which may only be used with an MSG rectifier, the values of the and the apply for operation with an MSG rectifier; i.e. the for overexcitation or the for electronic circuit interruption on the DC side.

The values for W_{L} are guidelines; actual values may vary significantly depending on the application situation. Periodic inspection of the air gap or brake disc thickness is recommended.

Actual response times may differ from the times listed here due to the effects of operating temperature, brake disc wear and manufacturing tolerances.

Key to symbols

- M_{Br} Rated braking torque
- WmaxMaximum allowable friction energy for an emergency stop with a holding brakeWmaxMaximum allowable friction energy for each brake cycle with working brakes
- WmaxMaximum allowable friction energy for each bWthMaximum allowable braking energy per hour
- WL Maximum allowable braking energy until maintenance; i.e. brake disc replacement or air gap adjustment. Air gap adjustment is possible only with type ZSXxx brakes.
- H∟ Manual release
- Response time for release with normal excitation.
 Overexcitation with a type MSG special rectifier reduces the response time by approximately 50 %.
- tac Response time for brakes with AC-side switch-off, i.e. by switching off the supply voltage to a separately powered standard rectifier. If the supply voltage for the rectifier is taken from the motor terminals, considerably longer response times should be expected (depending on the motor size and winding design).
- tocResponse time for braking with DC-side circuit interruption by
a mechanical switch.
In the case of electronic circuit interruption on the DC side by a
type ESG or MSG special rectifier, the response times will be approximately
two to three times as long.PelElectromagnet coil power consumption at 20 °C.
- Depending on the rated voltage of the coil, the actual power may differ from the guideline value stated here.
- J Moment of inertia of the drive bush and brake disc(s)

Brake

Connection

The electrical connections to the brake are made in the motor terminal box using terminals or the rectifier. Standard voltages:

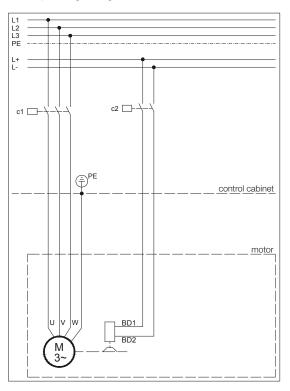
380–420 V 50/60 Hz (brake coil voltage 180 V DC)

220–230 V 50/60 Hz (brake coil voltage 105 V DC) 24 V DC (brake coil voltage 24 V DC)

Other voltages are available at additional cost.

DC connection via terminals (K)

The brake must be connected via separate terminals in the motor or brake terminal box directly to the DC voltage. The standard voltages are 180 V DC, 105 V DC and 24 V DC. Brakes with other operating voltages are available at additional cost.



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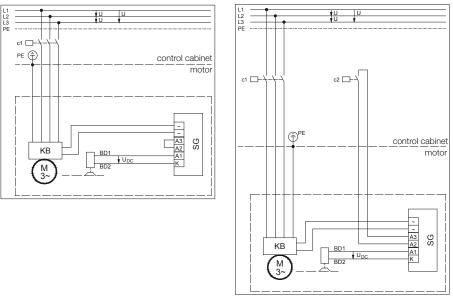
Half-wave rectifier with switch contacts for

Standard rectifier (S)

Working principle

	DC-side circuit interruption
Input voltage U1	max. 575 VAC +5 %
Output voltage	0.45 x U ₁ VDC
Max. output current	2.5 A DC
Ambient temperature	-40 to +40 °C
Connection	Caged Clamp terminals with clamp lever
Clampable conductor cross-section	max. 1.5 mm ² without wire end sleeve
	max. 1.5 mm ² with wire end sleeve
Approvals	c-CSA-us
	c-UL-us (only in combination with B2000 geared
	motors and brakes in the ES(X) or ZS(X) product series

The brake must be connected to the AC supply via the standard rectifier in the motor terminal box or brake terminal box. The standard voltages are 380 ... 420 V 50/60 Hz or 220 ... 230 V 50/60 Hz. Other voltages up to 575 V are available at extra cost. In a configuration with standard rectifier, the brake circuit can be interrupted by an extra contact on the d.c. side in order to reduce the response time. This significantly reduces the braking time and overtravel distance.



Voltage connection for the rectifier from the motor terminal block or cage clamp (see Rectifier Connection on Motor Terminal Block or Cage Clamp)

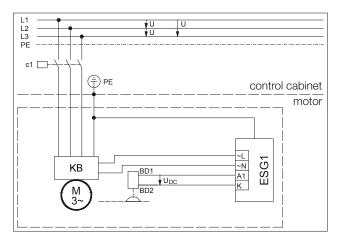
Rectifier for electronic rapid shutdown (E)

/n Working principle

DC-side circuit interruptionInput voltage U1220-460 V AC ±5 %, 50/60 HzOutput voltage0.45 x U1 V DCMax. output current1 A DCAmbient temperature-20 °C to +40 °CClampable conductor cross-sectionmax. 1.5 mm²

This rectifier permits electronic DC-side interruption of the brake circuit. No additional cable to the rectifier is necessary. The rectifier is supplied complete with a protective resistor which prevents a mains short- circuit via the shutdown arc of the high-speed motor contactor. Brake response times are significantly shorter than those achievable by AC-side interruption of the brake circuit. They are, however, longer than those achievable with DC-side interruption by a mechanical switch. The brake must be connected to the alternating current via the rapid shutdown rectifier in the motor terminal box or the brake terminal box. The standard voltages are 380 ... 420 V 50/60 Hz or 220 ... 230 V 50/60 Hz. Other voltages up to 460 V are available at extra cost.

Half-wave rectifier with electronic



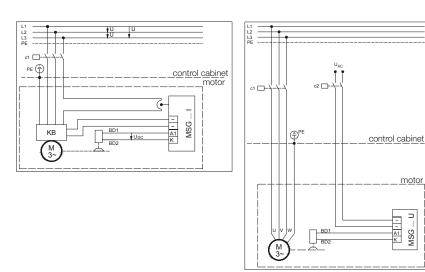
Voltage connection for the rectifier from the motor terminal block or cage clamp (see Rectifier Connection on Motor Terminal Block or Cage Clamp)

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Standard rectifier (M)

Working principle	MSG 1.5.4801 Half-wave rectifier with time-limited overexcitation and electronic DC-side circuit interruption
Input voltage U1	Fast shutdown due to no motor current in one phase 220–480 V AC +6 / -10 %, 50/60 Hz
Output voltage	$0.9 \times U_1 \text{ V DC}$ during overexcitation
	$0.45 \times U_1 \text{ V DC}$ over overexcitation period
Overexcitation time	0.3 s
Max. output current	1.5 A DC
Ambient temperature Clampable	-20 °C to +40 °C
conductor cross-section	max. 1.5 mm ²
Working principle	MSG 1.5.500U
Working principle	Half-wave rectifier with time-limed overexcitation and
Working principle	Half-wave rectifier with time-limed overexcitation and electronic DC-side circuit interruption
	Half-wave rectifier with time-limed overexcitation and electronic DC-side circuit interruption Fast shutdown due to the absence of input voltage
Input voltage U1	Half-wave rectifier with time-limed overexcitation and electronic DC-side circuit interruption Fast shutdown due to the absence of input voltage 220–500 V AC ± 10 %, 50/60 Hz
	Half-wave rectifier with time-limed overexcitation and electronic DC-side circuit interruption Fast shutdown due to the absence of input voltage 220–500 V AC ± 10 %, 50/60 Hz 0.9 x U ₁ V DC during overexcitation
Input voltage U ₁ Output voltage	Half-wave rectifier with time-limed overexcitation and electronic DC-side circuit interruption Fast shutdown due to the absence of input voltage 220–500 V AC ± 10 %, 50/60 Hz 0.9 x U ₁ V DC during overexcitation 0.45 x U ₁ V DC over overexcitation period
Input voltage U ₁ Output voltage Overexcitation time	Half-wave rectifier with time-limed overexcitation and electronic DC-side circuit interruption Fast shutdown due to the absence of input voltage 220–500 V AC ± 10 %, 50/60 Hz 0.9 x U ₁ V DC during overexcitation 0.45 x U ₁ V DC over overexcitation period 0.3 s
Input voltage U ₁ Output voltage	Half-wave rectifier with time-limed overexcitation and electronic DC-side circuit interruption Fast shutdown due to the absence of input voltage 220–500 V AC ± 10 %, 50/60 Hz 0.9 x U ₁ V DC during overexcitation 0.45 x U ₁ V DC over overexcitation period
Input voltage U ₁ Output voltage Overexcitation time	Half-wave rectifier with time-limed overexcitation and electronic DC-side circuit interruption Fast shutdown due to the absence of input voltage 220–500 V AC ± 10 %, 50/60 Hz 0.9 x U ₁ V DC during overexcitation 0.45 x U ₁ V DC over overexcitation period 0.3 s
Input voltage U ₁ Output voltage Overexcitation time Max. output current Ambient temperature Clampable	Half-wave rectifier with time-limed overexcitation and electronic DC-side circuit interruption Fast shutdown due to the absence of input voltage $220-500 V AC \pm 10 \%$, $50/60 Hz$ $0.9 \times U_1 V DC$ during overexcitation $0.45 \times U_1 V DC$ over overexcitation period 0.3 s 1.5 A DC -20 °C to $+40 °C$
Input voltage U ₁ Output voltage Overexcitation time Max. output current Ambient temperature	Half-wave rectifier with time-limed overexcitation and electronic DC-side circuit interruption Fast shutdown due to the absence of input voltage $220-500 V AC \pm 10 \%$, $50/60 Hz$ $0.9 x U_1 V DC$ during overexcitation $0.45 x U_1 V DC$ over overexcitation period 0.3 s 1.5 A DC

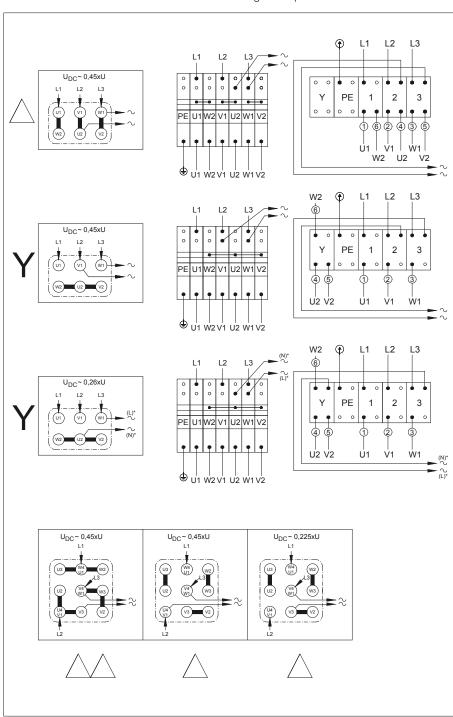
In cases where there are high motor switching frequencies, the brake can be de-energised more rapidly with this rectifier thereby significantly reducing the thermal stress on the motor. In addition, interrupting the brake's DC circuit by electronic means significantly reduces response times. Depending on the circumstances in which they are to be used, either the MSG 1.5.500 U (rapid shutdown brought about by removed supply voltage) or MSG 1.5.480 I (rapid shutdown brought about by removed motor current in a phase) is used. Power supply 220 to 480 V AC.



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motor

MSG ... U ~ ~ A1 K



Rectifier Connection on Motor Terminal Block or Cage Clamp

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Brake connection, operation with frequency converter	The voltage present at the motor terminal block when operating with a frequency converter is frequency-dependent. Brakes require a constant voltage, so they need a seperate electrical connection. This is the reason why the brake is not connected to the motor terminals ex- works.
Brake connection, pole-changing motors	The brakes of pole-changing motors need a seperate electrical connection. As is the case with motors for operation with frequency inverters, the brake is not connected to the motor terminals ex-works.
Manual release (HA, HN)	All brakes are available with mechanical manual release on request. Non-latching manual re- lease is the standard version (HN). A latching manual release (HA) can be supplied if required for all brake sizes.
Explosion protection	Brakes for use in hazardous areas are subject to special regulations. Please consult our sup- port specialists in these special cases.
Back stop (RR, RL)	Motors of size D08 to D22 are available with backstop. The locking rotational direction clockwise (RR) or anticlockwise (RL) is to given in the order. The reference is the connection side of the gearbox. Should the connection side not be clearly defined, gearbox side "V" (front) will be assumed (see chapter 17 Dimensions drawing "Motor with back stop").
	Note that the back-stop functionality on a motor operating with a frequency converter is guar- anteed only at rotor speeds above 740/min.
	It is advisable to consult BAUER for applications in corrosive atmospheres, especially for mo- tor-down installed positions.

Second motor shaft extension (ZW, ZV)	The motors are also available on request with a second motor shaft extension in design ZW (shaft with key) or ZV (shaft with square end).
	Half the central motor's rated power is available at each of the two shafts. Permissible radial loads available on request. Guards are not included in the scope of supply (for dimensional drawing see chapter 16).
	Motors with brakes are available on request with a second shaft stub extended through the brake.
Protective fan cowl (D)	A protective hood over the fan cowl is recommended for outdoor installations where the motor is pointing upward and subject to severe or prolonged exposure to water (dimensional drawing, see chapter 16).
	This protective hood is mandatory for upright explosion-proof motors.
	A special fan cowl for the textiles industry is available on request at extra cost. This design prevents airborne fibres and fluff clogging the fan cowl.
Motor-independent fan (FV)	For special applications, standard motors and brake motors of size D08 and larger are available with externally mounted motor-independent fans. The standard line voltage of the motor-independent fan matches the voltage of the geared motor (dimensional drawing for motor-independent fan, see chapter 16).
	The independent fans are supplied as standard with Bayonet-fitting for standard motors sizes D16 and D18 and brake motors sizes D11 to D18.

Technical Data:

Multivolt Conception Running capacitor for single phase duty enclosed as standard.

Technical Data Motor-independent fan

Mode Frame size		Blower Diameter	neter Range of voltage		max. permi	ssible current	max. power input		
IVIOde	Frame size	[mm]	[V]	[A]	[W]		
			50 Hz	60 Hz	50 Hz	60 Hz	50 Hz	60 Hz	
	63	118	230-277	230-277	0.18	0.21	46	54	
	71	132	230-277	230-277	0.18	0.21	48	56	
	80	150	230-277	230-277	0.19	0.22	48	59	
1 (()	90	169	220-277	220-277	0.29	0.23	59	61	
1 ~ ⊥ (∆)	100	187	220-277	220-277	0.29	0.28	62	73	
	112	210	220-277	220-277	0.27	0.36	64	88	
	132	250	230-277	230-277	0.52	0.61	125	163	
	160-200	300	230-277	230-277	1.05	1.52	246	390	
	63	118	346-525	380-575	0.09	0.08	28	29	
	71	132	346-525	380-575	0.09	0.07	29	28	
	80	150	346-525	380-575	0.09	0.07	33	36	
3 ~ Y	90	169	346-525	380-575	0.22	0.18	78	71	
3~Y	100	187	346-525	380-575	0.21	0.18	80	80	
	112	210	346-525	380-575	0.2	0.17	87	93	
	132	250	346-525	380-575	0.37	0.32	160	180	
	160-200	300	346-525	380-575	0.74	0.62	314	391	
	63	118	200-303	220-332	0.15	0.14	28	29	
	71	132	200-303	220-332	0.15	0.13	29	28	
	80	150	200-303	220-332	0.16	0.13	33	36	
0	90	169	200-303	220-332	0.39	0.32	78	71	
3 ~ Δ	100	187	200-303	220-332	0.37	0.3	80	80	
	112	210	200-303	220-332	0.35	0.29	87	93	
	132	250	200-303	220-332	0.64	0.55	160	180	
	160-200	300	200-303	220-332	1.28	1.08	314	391	

Motor Mounted Components Encoder System

Shaft encoder (G)

Bauer gear motors can be fitted with either an incremental encoder or an absolute encoder for special applications. Both the standard incremental encoder and the absolute encoder are optimised and suitable for use with all modern inverters.

Bauer standard encoders as from motor frame size D05 (0,18 kW) are protected against mechanical damage by means of a protective cover (Additional Dimension Sheet see chapter 16).

Special features: standard incremental encoder:

- Robust mount
- EMC-tested
- Protected against polarity reversal
- Supply voltage 8-30 V DC
- A-, B- and N-lines and inverted signals or output signals as preferred
- HTL output circuit (TTL on request)
- 1024 pulses per revolution

Special features: standard absolute encoder

- Steps per revolution: 8192 (13 Bit)
- Number of turns: 4096 (12 Bit) shaft turns
- Execution of electronic: SSI (Synchronous-Serial Interface)
- Output code: Gray-Code
- Supply voltage: 11-27 V DC
- Loss efficiency (no load): ≤ 3 Watt
- Output driver: RS-422 (2-wire)

Incremental rotary encoder

Functional description



Incremental encoders are used to determine motor shaft positions. An incremental encoder detects rotary motion and coverts it into an electrical output signal. An encoder disc with a specific number of periods per rotation senses angular motion. The optoelectronic scanning unit generates signals and issues pulses after the signals have been processed in trigger stages. The resolution is defined by the number of opaque and clear segments on the encoder disc. For example, an encoder with 1024 lines will generate a sequence of 1024 pulses for one full rotation.

The combination of an incremental encoder and a frequency converter allows optimised solutions to be developed, such as

- speed controllers with a wide adjustment range
- accurate speed control
- constant-speed control
- position control

Supply voltage:

Output signals: Pulses per revolution:

Enclosure rating: Temperature range: 8–30 V DC with HTL 5 V DC with differential TTL HTL A, B and N tracks; optional TTL 1024 Optional 1...65536 IP65 (optional IP67) -40 °C to +100 °C

Electrical specifications

Output voltage	RS 422 (TTL compatible)	RS 422 (TTL compatible)	Differential	Differential (7272)
Supply voltage	5–30 V DC	5 V ±5%	8–30 V DC	5–30 V DC
No-load current consumption With inversion:	max. 70 mA	max. 70 mA	max. 70 mA	max. 70 mA
Allowable load per channel:	max. ±20 mA	max. ±20 mA	max. ±20 mA	max. ±20 mA
Pulse rate:	max. 300 kHz	max. 300 kHz	max. 160 kHz	max. 160 kHz
High signal level:	min. 2.5 V	min. 2.5 V	min. UB – 3 V	min. UB – 3 V
Low signal level:	max. 0.5 V	max. 0.5 V	max. 1 V	max. 1 V

Plug end view with male pin insert

Connector type	8-pin M12 plug	12-pin M23 plug	MIL connector 10-pin
Layout	4 4 7		
Order code:	8.5000.XXX3.XXXX 8.5000.XXX4.XXXX	8.5000.XXX7.XXXX 8.5000.XXX8.XXXX	8.5000XXXY.XXXX
Mating 05.CMB-8181 connector:	-0	8.0000.5012.0000	8.0000.5062.0000

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Signal assignments

Signal:	0 V GND	+U _B	0 V Sens	+Ub Sens	А	А	В	В	Z	Z	Shield
M23 Multifast, 12-pin connector; pin assignments:	10	12	11	2	5	6	8	1	3	4	1)
M12 Eurofast, 8-pin connector; pin assignments:	1	2			3	4	5	6	7	8	1)
Military version; 10-pin connector; pin assignments:	F	D		E	А	G	В	Н	С	1	J ¹)
Cable; lead colour:	WH	BN	GY PK	RD BU	GN	YE	GY	PK	BU	RD	Shield

¹ Shield connected to plug housing.

Insulate unused outputs before putting into service.

Motor Mounted Components Absolute rotary encoders

Functional description

Profibus DP interface



cal signals. In contrast to incremental encoders, with absolute encoders the current position is directly available. If an absolute encoder is moved mechanically while it is switched off, after the power is switched on again the current position can be read out immediately and directly. Absolute encoders are available in single-turn and multi-turn versions.

Absolute encoders detect both angular and rotational motions and convert them into electri-

Specifications

Supply voltage No-load current consumption Total resolution ¹ Number of steps per revolution, standard/extended ¹ Number of turns, standard/extended ¹ Profibus DP V0 PNO encoder profile parameters ¹ Output code ¹

Advess Baud rate TR-specific functions ¹ Data width on bus for actual position Permissible mechanical speed Shaft load Bearing life - speed - operating temperature Shaft diameter [mm] Permissible angular acceleration Moment of inertia Start-up torque at 20 °C Weight

11-27 VDC < 350 mA ≤ 33 bits ≤ 8,192 / ≤ 32,768 ≤ 4,096 / ≤ 256,000 IEC 61158, IEC 61784 Class 1/Class 2 Counting direction switchover, scaling function, etc. Binary, Gray, truncated Gray 3-99, set using a rotary switch 9.6 kbit/s to 12 Mbit/s Gear and speed outputs ≤ 25 bits ≤ 12,000 rpm Own mass \geq 3.9 x 10¹⁰ revolutions at ≤ 6,000 rpm $\leq 60 \ ^{\circ}C$ 10H7 $\leq 10^4 \text{ rad/s}^2$ 2.5 x 10⁻⁶ kg m² (typical) 2 Ncm (typical) 0.3–0.5 kg

1) Configurable parameter

Ambient conditions

2 With mating connector fitted and/or cable glands fitted and tightened

Absolute rotary encoders

SSI interface



Specifications

Supply voltage No-load current consumption Total resolution ¹ Number of steps per revolution ¹ Number of rotations, standard ¹ Number of rotations, extended ¹ SSI Clock input Data output Clock frequency Monostable time t_M Output code ¹ Output format ¹

Negative values ¹ SSI or parallel special bits ¹

F/R ¹ Preset ¹ Logic levels Permissible mechanical speed Shaft load Bearing life - speed - operating temperature Shaft diameter [mm] Permissible angular acceleration Moment of inertia Start-up torque at 20 °C Weight Optional - incremental signals, RS422 levels

11-27 VDC < 350 mA \leq 25 bits ≤ 8,192 ≤ 4,096 ≤ 256,000 Synchronous Serial Interface Optocoupler RS-422, 2-wire 80 kHz – 1 MHz $16 \ \mu s \le t_M \le 25 \ \mu s$ (20 $\ \mu s$ typical) Binary, Gray, BCD Standard, Tannenbaum, SSI + CRC, 26-bit cycle, variable number of data bits Sign and magnitude, twos complement Limit switch, overspeed, direction indication, motion indication, error indication, parity Counting direction Electronic alignment "0" < +2 VDC; "1" = supply voltage ≤ 12,000 rpm Own mass \geq 3.9 x 10¹⁰ revolutions at ≤ 6,000 rpm ≤ 60 °C 10H7 $\leq 10^4 \text{ rad/s}^2$ 2.5 x 10⁻⁶ kg m² (typical) 2 Ncm (typical) 0.3-0.5 kg

K1+, K1-, K2+, K2- with 1024 or 2048 pulses

¹⁾ Configurable parameter

Ambient conditions

 $\begin{array}{lll} \mbox{Vibration (EN 60068-2-6:1996)} &\leq 100\mbox{ m/s}^2,\mbox{ sinusoidal 50-2,000\ Hz} \\ \mbox{Shock (EN 60068-2-27:1995)} &\leq 1000\mbox{ m/s}^2,\mbox{ half-cycle sinusoidal 11\ ms} \\ \mbox{EMC} \\ & - \mbox{ Interference emission compliant with EN 61000-6-3:2007} \\ & - \mbox{ Interference immunity compliant with EN 61000-6-2:2006} \\ \mbox{Operating temperature} & 0\ ^\circ\mbox{C to } +60\ ^\circ\mbox{C; optionally } -20\ ^\circ\mbox{C to } +70\ ^\circ\mbox{C} \\ \mbox{Storage temperature} & -30\ ^\circ\mbox{C to } +80\ ^\circ\mbox{C, dry} \\ \mbox{Relative humidity (EN 60068-3-4:2002) 98\ \%,\ non\ condensing} \\ \mbox{Enclosure rating (EN 60529:1991)}^2 & \mbox{IP65} \\ \end{array}$

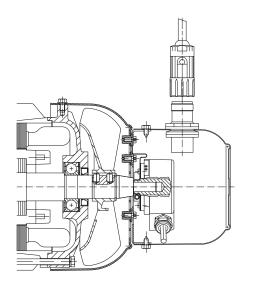
²⁾ With mating connector fitted and/or cable glands fitted and tightened

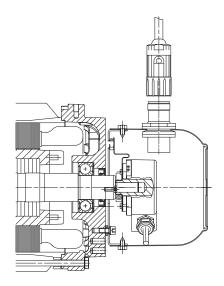
In addition to the angular position within a rotation, multiturn encoders detect multiple rotations. An internal reduction gear mechanism connected to the motor shaft is used to detect the number of turns. Consequently, the value measured by a multiturn encoder consists of the current angular position and the number of turns. As with incremental encoders, the reading is calculated and output via various interface modules, depending on the interface.

On request, a large range of motor frames can be fitted with sensor bearings. The output signal from the sensor allows the direction of rotation to be determined, among other things. The number of possible pulse counts depends on the frame size. Please enquire for more information.

Motor Mounted Components Modular Motorsystem

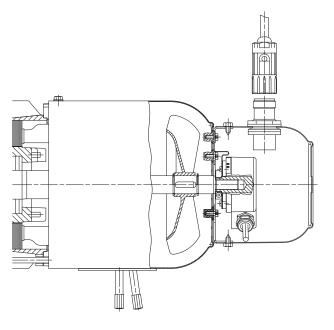
Motor and encoder

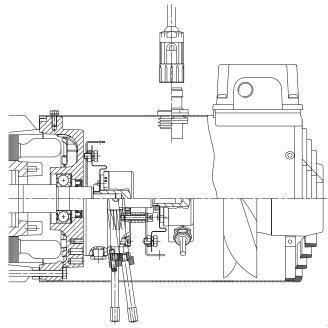




Motor, brake and encoder

Motor and forced ventilation





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Energy Efficient Geared Motors AC Line Operated